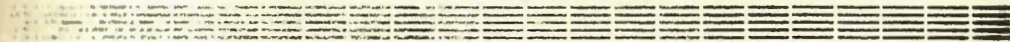


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ЕРЕВАНСКИЙ ФИЗИЧЕСКИЙ ИНСТИТУТ
YEREVAN PHYSICS INSTITUTE



THE FORMULAE FOR THE SEMI-ANALYTICAL CALCULATIONS
OF THE FIELDS IN CYLINDRICAL APERIODIC STRUCTURES

AMBARTSUMIAN V.G.

Формулы для полуаналитических расчетов полей в
цилиндрических аперiodических структурах.

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THE FORMULAE FOR THE SEMI-ANALYTICAL CALCULATIONS
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ABSTRACT

Formulae are derived to calculate the fields in a cylindrical aperiodic structure. Account is taken also of the fields excited by the accelerated beam moving at a velocity $v \approx c$ parallel to the structure's axis. The formulae are obtained by the field-matching method and expressed using the "transfer" matrices.

Yerevan Physics Institute

The formulae for the semi-analytical calculations of the
fields in cylindrical aperiodic structures

It is known that the next generations of the linear accelerators of charged particles are distinguished by the high acceleration rates ($\sim 100 \text{ MeV/m}$) and large currents of accelerated particles ($\sim 100 \text{ mA}$). This circumstance requires the use of high frequency accelerating fields ($\sim 10\text{--}20 \text{ GHz}$) and accelerating structures with the compact cells (a few cm). But the large currents of charge and small sizes of the cells lead to the effects of beam breakup. At present it is known two methods for suppression of these effects: the damping method and detuned structure [1].

In [2] the formulae had been derived and carried out the semi-analytical calculations of fields in detuned (aperiodic) cylindrical structures for the symmetrical spatial electric modes ($m=0$). A slightly different way is chosen in [3] to derive formulae for the field calculations at the same case ($m=0$).

In this work we carry out the derivation of formulae for the semi-analytical calculations of fields in structures which consist the cylindrical cells with the arbitrary sizes (Fig.1) in the case of arbitrary spatial mode (arbitrary m), the special case for which is the structure described in [2].

1. The expansion of fields

The general solution of Maxwell equations in the arbitrary

N_{th} cell we represent as a sum of two solutions: particular solution of inhomogeneous equations and general solution of homogeneous equations. We will not consider here the inhomogeneous solution in detail, because it depends on the concrete distribution of current of the accelerated charges, but we assume that it satisfies the boundary conditions $E_{\perp}^a = 0$ on the cylindrical walls of cell. In appendix we derive the inhomogeneous solution for the important practical case at which point-like charged bunch moves parallel to the structures axis with the small offset $\delta r^a \ll a^N$ (a^N is the radius of N th cell).

Now we proceed to the homogeneous solution. The Fourier harmonics of homogeneous solution on the frequency ω can be found using electric and magnetic Hertz vectors which have only two non-zero components $\vec{\Phi}_z^{E,N}$ and $\vec{\Phi}_z^{H,N}$ for our case.

Thus \vec{E}^N and \vec{H}^N can be found according to expressions:

$$\vec{E}^N = \nabla(\nabla \vec{\Phi}_z^{E,N}) + \tilde{k}^2 \vec{\Phi}_z^{E,N} + i\tilde{k}[\nabla \vec{\Phi}_z^{H,N}] \quad 1.1$$

$$\vec{H}^N = -i\tilde{k}[\nabla \vec{\Phi}_z^{E,N}] + \nabla(\nabla \vec{\Phi}_z^{H,N}) + \tilde{k}^2 \vec{\Phi}_z^{H,N} \quad 1.2$$

where $\vec{\Phi}_z^{E,N}$ and $\vec{\Phi}_z^{H,N}$ are solutions of wave equation:

$$\Delta \vec{\Phi}_z^{E(H),N} + \tilde{k}^2 \vec{\Phi}_z^{E(H),N} = 0; \quad \vec{\Phi}_z^{E(H),N} = \vec{\Phi}_\varphi^{E(H),N} = 0; \quad \tilde{k} = \frac{\omega}{c} \quad 1.3$$

$$\vec{\Phi}_z^{E,N} = \sum_{m,k} \vec{\Phi}_{mk}^{E,N} (\vec{C}_{mk}^{E,N} e^{ih_{mk}^E z} + \vec{C}_{mk}^{E,N} e^{-ih_{mk}^E z}) + \sum_{m,k} \vec{\Phi}_{mk}^{E,N} (\vec{C}_{mk}^{E,N} e^{ih_{mk}^E z} + \vec{C}_{mk}^{E,N} e^{-ih_{mk}^E z}) \quad 1.4$$

$$\vec{\Phi}_z^{H,N} = \sum_{m,k} \vec{\Phi}_{mk}^{H,N} (\vec{C}_{mk}^{H,N} e^{ih_{mk}^H z} - \vec{C}_{mk}^{H,N} e^{-ih_{mk}^H z}) + \sum_{m,k} \vec{\Phi}_{mk}^{H,N} (\vec{C}_{mk}^{H,N} e^{ih_{mk}^H z} - \vec{C}_{mk}^{H,N} e^{-ih_{mk}^H z}) \quad 1.5$$

$$\left. \begin{aligned} \vec{\Phi}_{mk}^{E(H),N} &= J_m(g_{mk}^{E(H),N} z) \cos(m\varphi) \\ \vec{\Phi}_{mk}^{E(H),N} &= J_m(g_{mk}^{E(H),N} z) \sin(m\varphi) \end{aligned} \right\} \quad 1.6$$

$$\left. \begin{aligned} h_{mk}^{E(H),N} &= \sqrt{\tilde{k}^2 - g_{mk}^{E(H),N}} \quad \text{npu} \quad \tilde{k}^2 - g_{mk}^{E(H),N} \geq 0 \\ h_{mk}^{E(H),N} &= i\sqrt{g_{mk}^{E(H),N} - \tilde{k}^2} \quad \text{npu} \quad \tilde{k}^2 - g_{mk}^{E(H),N} < 0 \end{aligned} \right\} \quad 1.7$$

$$g_{mk}^{E,N} = \frac{V_{mk}}{a^N}; \quad g_{mk}^{H,N} = \frac{M_{mk}}{a^N}; \quad J_m(V_{mk}) = J_m'(M_{mk}) = 0$$

Here J_m are Bessel functions, $\vec{C}_{mk}^{E(H),N}$ are constants. The sign (-) before the second terms of sum (1.5) and also the correspondences $c \leftrightarrow s, s \leftrightarrow c$ are chosen for convenience. The functions $\vec{\Phi}_{mk}^{E(H),N}$ already satisfy the continuity conditions on the cylindrical walls of cells. For convenience we introduce the usual notations:

$$\chi_{mk}^{E(H),N}(z) = \vec{C}_{mk}^{E(H),N} e^{ih_{mk}^{E(H),N} z} + \vec{C}_{mk}^{E(H),N} e^{-ih_{mk}^{E(H),N} z} \quad 1.8$$

$$y_{mk}^{E(H),N}(z) = \frac{d \chi_{mk}^{E(H),N}(z)}{dz} \quad 1.9$$

According to the (1.1, 1.2) for the fields inside the N th cell we have:

$$E_z^N(\varphi, z, \tilde{k}) = \sum_{m,k} g_{mk}^{E,N} [\vec{\Phi}_{mk}^{E,N} \chi_{mk}^{E,N}(z) + \vec{\Phi}_{mk}^{E,N} \chi_{mk}^{E,N}(z)] \quad 1.10$$

$$E_\varphi^N(\varphi, z, \tilde{k}) = \sum_{m,k} [\vec{\Phi}_{mk}^{E,N} y_{mk}^{E,N}(z) + \vec{\Phi}_{mk}^{E,N} y_{mk}^{E,N}(z)] \quad 1.11$$

$$E_\varphi^N(\varphi, z, \tilde{k}) = \frac{1}{2} \sum_{m,k} m [\vec{\Phi}_{mk}^{E,N} y_{mk}^{E,N}(z) - \vec{\Phi}_{mk}^{E,N} y_{mk}^{E,N}(z)] \quad 1.12$$

$$H_z^{E,N}(\varphi, z, z, \tilde{k}) = 0 \quad 1.13$$

$$H_z^{E,N}(\varphi, z, z, \tilde{k}) = \frac{i\tilde{k}}{2} \sum_{m,k} m \left[\tilde{\Phi}_{mk}^{E,N} \chi_{mk}^{E,N}(z) + \tilde{\Phi}_{mk}^{E,N'} \chi_{mk}^{E,N}(z) \right] \quad 1.14$$

$$H_\varphi^{E,N}(\varphi, z, z, \tilde{k}) = -i\tilde{k} \sum_{m,k} \left[\tilde{\Phi}_{mk}^{E,N} \chi_{mk}^{E,N}(z) + \tilde{\Phi}_{mk}^{E,N'} \chi_{mk}^{E,N}(z) \right] \quad 1.15$$

$$E_z^{H,N}(\varphi, z, z, \tilde{k}) = 0 \quad 1.16$$

$$E_z^{H,N}(\varphi, z, z, \tilde{k}) = \frac{\tilde{k}}{2} \sum_{m,k} \frac{m}{h_{m,k}^{H,N}} \left[\tilde{\Phi}_{mk}^{H,N} \chi_{mk}^{H,N}(z) - \tilde{\Phi}_{mk}^{H,N'} \chi_{mk}^{H,N}(z) \right] \quad 1.17$$

$$E_\varphi^{H,N}(\varphi, z, z, \tilde{k}) = \tilde{k} \sum_{m,k} \frac{1}{h_{m,k}^{H,N}} \left[\tilde{\Phi}_{mk}^{H,N} \chi_{mk}^{H,N}(z) + \tilde{\Phi}_{mk}^{H,N'} \chi_{mk}^{H,N}(z) \right] \quad 1.18$$

$$H_z^{H,N}(\varphi, z, z, \tilde{k}) = -i \sum_{m,k} \frac{g_{mk}^{H,N}}{h_{m,k}^{H,N}} \left[\tilde{\Phi}_{mk}^{H,N} \chi_{mk}^{H,N}(z) + \tilde{\Phi}_{mk}^{H,N'} \chi_{mk}^{H,N}(z) \right] \quad 1.19$$

$$H_z^{H,N}(\varphi, z, z, \tilde{k}) = i \sum_{m,k} h_{m,k}^{H,N} \left[\tilde{\Phi}_{mk}^{H,N} \chi_{mk}^{H,N}(z) + \tilde{\Phi}_{mk}^{H,N'} \chi_{mk}^{H,N}(z) \right] \quad 1.20$$

$$H_\varphi^{H,N}(\varphi, z, z, \tilde{k}) = \frac{i}{2} \sum_{m,k} m h_{m,k}^{H,N} \left[\tilde{\Phi}_{mk}^{H,N} \chi_{mk}^{H,N}(z) + \tilde{\Phi}_{mk}^{H,N'} \chi_{mk}^{H,N}(z) \right] \quad 1.21$$

Here by the prime we mark the derivative with respect to r .

2. The continuity conditions

The continuity conditions for the fields on the transverse walls of cells at $z=0$ and $z=l^N$ are:

$$\tilde{E}_z^N(\varphi, z, e^N, \tilde{k}) = \tilde{E}_z^{N+1}(\varphi, z, 0, \tilde{k}) \quad 0 \leq z \leq a_2^N \quad 2.1$$

$$\tilde{E}_r^N(\varphi, z, e^N, \tilde{k}) \theta(a^N - r) = \tilde{E}_r^{N+1}(\varphi, z, 0, \tilde{k}) \theta(a^{N+1} - r) \quad 2.2$$

$$\tilde{E}_\varphi^N(\varphi, z, e^N, \tilde{k}) \theta(a^N - r) = \tilde{E}_\varphi^{N+1}(\varphi, z, 0, \tilde{k}) \theta(a^{N+1} - r) \quad 2.3$$

$$\vec{H}^N(\varphi, z, e^N, \tilde{k}) = \vec{H}^{N+1}(\varphi, z, 0, \tilde{k}) \quad 0 \leq z \leq a_2^N \quad 2.4$$

where for the two arbitrary quantities ρ^N and ρ^{N+1} we introduce the quantities ρ_1^N and ρ_2^N :

$$\left. \begin{aligned} \rho_1^N &= \rho^N \theta_1^N + \rho^{N+1} \theta_2^N \\ \rho_2^N &= \rho^N \theta_2^N + \rho^{N+1} \theta_1^N \\ \theta_1^N &\equiv \theta(a^N - a^{N+1}); \quad \theta_2^N \equiv \theta(a^{N+1} - a^N) \end{aligned} \right\} \quad 2.5$$

In (2.1+2.4) \vec{E} and \vec{H} are the total fields, l^N is the length of the N th cell. From (2.4), $\text{div} \vec{H} = 0$ follows the condition:

$$\frac{\partial \tilde{H}_z^N}{\partial z} / (\varphi, z, e^N, \tilde{k}) = \frac{\partial \tilde{H}_z^{N+1}}{\partial z} / (\varphi, z, 0, \tilde{k}) \quad 2.6$$

As it can be seen below, the conditions (2.1+2.3), (2.6) and boundary conditions at the structures both ends are sufficient for the unequal determination of fields inside the structure.

3. The fields matching

Multiplying (2.2) by $[r^{2c(s)} \tilde{\Phi}_{m,k}^{H,N}]_1$, (2.3) by $[r^{2c(s)} \tilde{\Phi}_{m,k}^{E,N}]_1$

and integrating from "0" to a_1^N , also multiplying (2.1) by $[r^{c(s)} \tilde{\Phi}_{m,k}^{E,N}]_2$, (2.4) by $[r^{c(s)} \tilde{\Phi}_{m,k}^{H,N}]_2$ and integrating from "0" to a_2^N we determine:

$$\begin{aligned} R_{m,2(\varphi),1}^{c(s)} E_{m,1}^{c(s)} + R_{m,2(\varphi),1}^{c(s)} H_{m,1}^{c(s)} &= R_{m,2(\varphi),2}^{c(s)} E_{m,2}^{c(s)} + \\ + R_{m,2(\varphi),2}^{c(s)} H_{m,2}^{c(s)} + P_{m,2(\varphi)}^{c(s)} E_{m,2}^{c(s)} & \quad 3.1 \end{aligned}$$

$$R_{m,2,1}^{(CS)} E_{m,1}^{(H),N} = R_{m,2,2}^{(CS)} E_{m,2}^{(H),N} + P_{m,2}^{(CS)} E_{m,2}^{(H),N} \quad 3.2$$

where

$$\left. \begin{aligned} P_{m,1(2)}^{(CS)} E_{m,1(2)}^{(H),N} &= \sum_m^{(CS)} E_{m,1(2)}^{(H),N} \mathcal{C}_{1(2)}^N + \sum_m^{(CS)} E_{m,1(2)}^{(H),N+1} \mathcal{C}_{2(1)}^N \\ E_{m,1(2)}^{(H),N} &= \sum_m^{(CS)} E_{m,1(2)}^{(H),N} \mathcal{C}_{1(2)}^N + \sum_m^{(CS)} E_{m,1(2)}^{(H),N+1} \mathcal{C}_{2(1)}^N \end{aligned} \right\} \quad 3.3$$

$$Y_m \equiv \begin{pmatrix} (Y_m)_1 \\ (Y_m)_2 \\ \vdots \end{pmatrix}; \quad X_m \equiv \begin{pmatrix} (X_m)_1 \\ (X_m)_2 \\ \vdots \end{pmatrix} \quad 3.4$$

The matrices R and vectors P are:

$$\left(R_{m,2,1}^{(CS)} \right)_{kn} = \frac{2J_m(V_{mn} \alpha_N) \alpha_N^2 V_{mn}^2}{(V_{mk}^2 - \alpha_N^2 V_{ml}^2) J_{m+1}(V_{mk}) V_{mk}} \quad 3.5$$

$$\left(R_{m,2,2}^{(CS)} \right)_{kn} = \delta_{kn} \quad 3.6$$

$$\left(R_{m,2,1}^{(H),N} \right)_{kn} = \frac{2J_m'(V_{mn} \alpha_N) \alpha_N^3 \mu_{mn}^3 h_{m,2,1}^{H,N}}{(\mu_{mk}^2 - \alpha_N^2 \mu_{mn}^2) (\mu_{mk}^2 - m^2) J_m(\mu_{mk}) h_{m,2,2}^{H,N}} \quad 3.7$$

$$\left(R_{m,2,2}^{(H),N} \right)_{kn} = \delta_{kn} \quad 3.8$$

$$\left(R_{m,2,1}^{(E),N} \right)_{kn} = -\frac{2J_{m+1}(V_{mn}) J_m(\mu_{mk}) V_{mn}^3}{(\mu_{mk}^2 - V_{mn}^2)^2} \quad 3.9$$

$$\left(R_{m,2,2}^{(E),N} \right)_{kn} = \frac{2J_m'(V_{mn}) J_m(\mu_{mk} \alpha_N) \alpha_N^2 V_{mn}^3}{(V_{mn}^2 - \mu_{mk}^2 \alpha_N^2)^2} + \frac{J_m'(\mu_{mk} \alpha_N) J_m'(V_{mn} \alpha_N) \alpha_N^3 V_{mn} \mu_{mk}}{(V_{mn}^2 - \mu_{mk}^2 \alpha_N^2)} \quad 3.10$$

$$\left(R_{m,2,1}^{(H),N} \right)_{kn} = -\left(R_{m,2,1}^{(H),N} \right)_{kn} = -\frac{m\tilde{K}}{2} \left(1 - \frac{m^2}{\mu_{mk}^2} \right) \frac{J_m^2(\mu_{mk})}{h_{m,2,1}^{H,N}} \delta_{kn} \quad 3.11$$

$$\left(R_{m,2,2}^{(H),N} \right)_{kn} = -\left(R_{m,2,2}^{(H),N} \right)_{kn} = -\frac{m\tilde{K}}{h_{m,2,2}^{H,N}} \frac{J_m'(\mu_{mk} \alpha_N) J_m(\mu_{mn} \alpha_N) \alpha_N^3 \mu_{mk}}{\mu_{mn}^2 - \mu_{mk}^2 \alpha_N^2} \quad 3.12$$

$$\left(R_{m,2,1}^{(E),N} \right)_{kn} = -\left(R_{m,2,1}^{(E),N} \right)_{kn} = -\frac{m}{2} J_{m+1}^2(V_{mk}) \delta_{kn} \quad 3.13$$

$$\left(R_{m,2,2}^{(E),N} \right)_{kn} = -\left(R_{m,2,2}^{(E),N} \right)_{kn} = m \frac{J_m'(V_{mn}) J_m(V_{mk} \alpha_N) V_{mn}}{V_{mn}^2 - V_{mk}^2 \alpha_N^2} \quad 3.14$$

$$\left(R_{m,2,1}^{(CS)} \right)_{kn} = \frac{2\tilde{K}}{h_{m,2,1}^{H,N}} \frac{J_m'(V_{mk}) J_m(\mu_{mn}) \mu_{mn}^2 V_{mk}}{(V_{mk}^2 - \mu_{mn}^2)^2} \quad 3.15$$

$$\left(R_{m,2,2}^{(CS)} \right)_{kn} = \frac{2\tilde{K} J_m'(V_{mk} \alpha_N) J_m(\mu_{mn}) \mu_{mn}^2 V_{mk} \alpha_N^3}{h_{m,2,2}^{H,N} (\mu_{mn}^2 - V_{mk}^2 \alpha_N^2)^2} + \frac{\tilde{K} J_m(V_{mk} \alpha_N) J_m(\mu_{mn}) (\mu_{mn}^2 - m^2) \alpha_N^2}{h_{m,2,2}^{H,N} (\mu_{mn}^2 - V_{mk}^2 \alpha_N^2)} \quad 3.16$$

$$P_{m,2}^{(CS)} = \frac{1}{\pi (a_1^N)^2} \int_0^{2\pi} \int_0^{a_1^N} \{ [E_2^Q]_2 \Theta(a_2^N - r) - [E_2^Q]_1 \} [\Phi_{mk}^{(CS)}]_1 r^2 dr d\varphi \quad 3.17$$

$$P_{m,2}^{(E),N} = \frac{1}{\pi (a_1^N)^2} \int_0^{2\pi} \int_0^{a_1^N} \{ [E_2^Q]_2 \Theta(a_2^N - r) - [E_2^Q]_1 \} [\Phi_{mk}^{(E),N}]_1 r^2 dr d\varphi \quad 3.18$$

$$P_{m,2}^{(CS)} = \frac{2}{\pi J_{m+1}^2(V_{mk}) (a_2^N)^2} \int_0^{2\pi} \int_0^{a_2^N} \{ [E_2^Q]_2 - [E_2^Q]_1 \} [\Phi_{mk}^{(CS)}]_2 r dr d\varphi \quad 3.19$$

$$P_{m,2}^{(H),N} = \frac{2}{\pi (a_2^N)^2 \left(1 - \frac{m^2}{\mu_{mk}^2} \right) J_m^2(\mu_{mk}) h_{m,2,2}^{H,N}} \times \int_0^{2\pi} \int_0^{a_2^N} \{ \left[\frac{\partial H_2^Q}{\partial z} \right]_2 - \left[\frac{\partial H_2^Q}{\partial z} \right]_1 \} [\Phi_{mk}^{(H),N}]_2 r dr d\varphi \quad 3.20$$

The quantities $h_{mn,1}^{H,N}$ and $h_{mn,2}^{H,N}$ are defined according to (2.5)

$$\text{and } \alpha_N = a_2^N / a_1^N.$$

Here \vec{E}^a and \vec{H}^a are the Fourier harmonics of inhomogeneous solution. Indexes "1" and "2" are defined according to (2.5).

For the quantities with the different indexes "E" and "H" we introduce the new vector :

$$\beta = \begin{pmatrix} \beta^E \\ \beta^H \end{pmatrix} \quad 3.21$$

For example, we can write for two vectors $\vec{\eta}_{m,1(2)}^{c(s)E(H),N}$:

$$\vec{\eta}_{m,1(2)}^{c(s)} = \begin{pmatrix} \vec{\eta}_{m,1(2)}^{c(s)E,N} \\ \vec{\eta}_{m,1(2)}^{c(s)H,N} \end{pmatrix} \quad 3.22$$

Let's introduce the following matrices:

$$\vec{T}_{m,1(2)}^{c(s)N} = \begin{pmatrix} R_{m,1(2)}^{c(s)E,N} ; R_{m,1(2)}^{c(s)H,N} \\ R_{m,1(2)}^{c(s)E,N} ; R_{m,1(2)}^{c(s)H,N} \end{pmatrix}; \quad \vec{S}_{m,1(2)}^{c(s)N} = \begin{pmatrix} R_{m,1(2)}^{c(s)E,N} ; 0 \\ 0 ; R_{m,1(2)}^{c(s)H,N} \end{pmatrix} \quad 3.23$$

Now we can rewrite (3.1) and (3.2) :

$$\vec{T}_{m,1}^{c(s)N} \vec{M}_{m,1}^{c(s)N} = \vec{T}_{m,2}^{c(s)N} \vec{M}_{m,2}^{c(s)N} + \vec{P}_m^{c(s)N} \quad 3.24$$

$$\vec{S}_{m,1}^{c(s)N} \vec{M}_{m,1}^{c(s)N} = \vec{S}_{m,2}^{c(s)N} \vec{M}_{m,2}^{c(s)N} + \vec{P}_m^{c(s)N} \quad 3.25$$

where

$$\vec{P}_m^{c(s)N} = \begin{pmatrix} P_{m,1}^{c(s)E,N} \\ P_{m,2}^{c(s)E,N} \\ P_{m,1}^{c(s)H,N} \\ P_{m,2}^{c(s)H,N} \end{pmatrix}; \quad \vec{P}_{m,2}^{c(s)N} = \begin{pmatrix} P_{m,1}^{c(s)E,N} \\ P_{m,2}^{c(s)E,N} \\ P_{m,1}^{c(s)H,N} \\ P_{m,2}^{c(s)H,N} \end{pmatrix} \quad 3.26$$

In the expression (3.25) we omit the matrices $\vec{S}_{m,2}^{c(s)N}$

because they are equal to unit matrices.

As follows from (3.25), at $m \neq 0$ in the structure cannot exist the fields purely of type "E" or purely of type "H".

Also, because $\text{Det}(\vec{S}_{m,1}^{c(s)N}) = 0$ (for the structure cannot exist the local transfer matrices), hereafter we shall proceed from the consequences of the theorem of the unequal determination of fields inside any volume at known \vec{E}_t or \vec{H}_t on the boundaries.

4. The basic relations

Before deriving the basic relations we introduce a few necessary notations and expressions.

From (3.24) we express $\vec{\eta}_{m,1}^{c(s)N}$ through $\vec{\eta}_{m,2}^{c(s)N}$ and $\vec{P}_m^{c(s)N}$:

$$\vec{\eta}_{m,1}^{c(s)N} = \vec{W}_m^{c(s)N} \vec{\eta}_{m,2}^{c(s)N} + \vec{V}_m^{c(s)N} \quad 4.1$$

where

$$\vec{W}_m^{c(s)N} = (\vec{T}_{m,1}^{c(s)N})^{-1} \vec{T}_{m,2}^{c(s)N}; \quad \vec{V}_m^{c(s)N} = (\vec{T}_{m,1}^{c(s)N})^{-1} \vec{P}_m^{c(s)N} \quad 4.2$$

Introduce the following matrices and vectors:

$$\vec{W}_m^{c(s)N} = \vec{\theta}_1^N + \vec{\theta}_2^N \vec{W}_m^{c(s)N}; \quad \vec{W}_m^{c(s)N} = \vec{\theta}_2^N + \vec{\theta}_1^N \vec{W}_m^{c(s)N} \quad 4.3$$

$$\vec{V}_m^{(c)} = \Theta_2^N \vec{V}_m^{(c)}; \quad \vec{V}_m^{(c)} = \Theta_1^N \vec{V}_m^{(c)} \quad 4.4$$

It is not difficult to verify that the following expressions hold:

$$\left. \begin{aligned} \vec{Y}_m^N(\ell^N) &= \vec{W}_m^N \vec{\eta}_{m,2}^N + \vec{V}_m^N \\ \vec{Y}_m^{N+1}(0) &= \vec{W}_m^N \vec{\eta}_{m,2}^N + \vec{V}_m^N \end{aligned} \right\} \quad 4.5$$

Introduce also the matrices $\tilde{\lambda}_{m,s}^N, \tilde{\lambda}_{m,t}^N$:

$$\tilde{\lambda}_{m,s}^N = \begin{pmatrix} \tilde{\lambda}_{E,N}^{(H,N)} & 0 \\ 0 & \tilde{\lambda}_{H,N}^{(H,N)} \end{pmatrix} \quad 4.6$$

$$\left(\tilde{\lambda}_{m,s}^{(H,N)} \right)_{kl} = \frac{\delta_{kl}}{i h_{mk}^{(H,N)} \operatorname{sh}(i h_{mk}^{(H,N)} \ell^N)} \quad 4.7$$

$$\left(\tilde{\lambda}_{m,t}^{(H,N)} \right)_{kl} = \frac{\delta_{kl}}{i h_{mk}^{(H,N)} \operatorname{th}(i h_{mk}^{(H,N)} \ell^N)} \quad 4.8$$

Using these matrices we can write:

$$\vec{X}_m^N(0) = \tilde{\lambda}_{m,s}^N \vec{Y}_m^N(\ell^N) - \tilde{\lambda}_{m,t}^N \vec{Y}_m^N(0) \quad 4.9$$

$$\vec{X}_m^N(\ell^N) = \tilde{\lambda}_{m,t}^N \vec{Y}_m^N(\ell^N) - \tilde{\lambda}_{m,s}^N \vec{Y}_m^N(0) \quad 4.10$$

Now we with the use of (3.3, 4.1, 4.5, 4.9, 4.10) all quantities in

(3.25) express in terms of $\vec{\eta}_{m,2}^{(c)N-1}, \vec{\eta}_{m,2}^{(c)N}, \vec{\eta}_{m,2}^{(c)N+1}$ and through free terms:

$$\vec{E}_m^N \vec{\eta}_{m,2}^{(c)N-1} + \vec{F}_m^N \vec{\eta}_{m,2}^{(c)N} + \vec{G}_m^N \vec{\eta}_{m,2}^{(c)N+1} + \vec{H}_m^N = 0 \quad 4.11$$

where

$$\vec{E}_m^N = (\Theta_2^N - \Theta_1^N \vec{S}_{m,1}^{(c)N}) \tilde{\lambda}_{m,s}^N \vec{W}_m^{(c)N-1} \quad 4.12$$

$$\vec{F}_m^N = \vec{S}_{m,1}^{(c)N} (\Theta_1^N \tilde{\lambda}_{m,t}^N - \Theta_2^N \tilde{\lambda}_{m,t}^{N+1}) \vec{W}_m^{(c)N} - (\Theta_2^N \tilde{\lambda}_{m,t}^N - \Theta_1^N \tilde{\lambda}_{m,t}^{N+1}) \quad 4.13$$

$$\vec{G}_m^N = (\Theta_2^N \vec{S}_{m,1}^{(c)N} - \Theta_1^N) \tilde{\lambda}_{m,s}^{N+1} \vec{W}_m^{(c)N+1} \quad 4.14$$

$$\vec{H}_m^N = \left\{ \vec{S}_{m,1}^{(c)N} \left[\Theta_1^N (\tilde{\lambda}_{m,t}^N \vec{V}_m^N - \tilde{\lambda}_{m,s}^{(c)N} \vec{V}_m^{N-1}) + \Theta_2^N (\tilde{\lambda}_{m,s}^{N+1} \vec{V}_m^{N+1} - \tilde{\lambda}_{m,t}^{(c)N} \vec{V}_m^N) \right] - (\Theta_1^N \tilde{\lambda}_{m,s}^{N+1} \vec{V}_m^{N+1} - \Theta_2^N \tilde{\lambda}_{m,s}^N \vec{V}_m^{N-1}) \right\} - \vec{P}_{m,2} \quad 4.15$$

The expressions (4.11) we call the basic relations. They are the consequences of the theorem of unequal determination of fields.

5. The boundary conditions and determination of the fields

We assume that at the ends of structure the quantities $\vec{C}_m^{(c)}$ and $\vec{C}_m^{(s)}$ are known (N_c is the number of the last cell).

From (4.11) we express the $\vec{\eta}_{m,2}^{(c)N-2}$ through $\vec{\eta}_{m,2}^{(c)N-3}$ and

$$\vec{\eta}_{m,2}^{(c)N-2} = \vec{A}_m^{(c)N-3} \vec{\eta}_{m,2}^{(c)N-3} + \vec{B}_m^{(c)N-3} + \vec{B}_m^{(s)N-3} \vec{\eta}_{m,2}^{(s)N-1} \quad 5.1$$

where

$$A_m^{c(s)N-3} = - (F_m^{c(s)N-2})^{-1} E_m^{c(s)N-2} \quad 5.2$$

$$B_m^{c(s)N-3} = - (F_m^{c(s)N-2})^{-1} H_m^{c(s)N-2} \quad 5.3$$

$$\hat{B}_m^{c(s)N-3} = - (F_m^{c(s)N-2})^{-1} G_m^{c(s)N-2} \quad 5.4$$

Now with the substitutions in (4.11) we obtain the recurrence formulae for $\eta_{m,2}^{c(s)N}$:

$$\eta_{m,2}^{c(s)M} = A_m^{c(s)M-1} \eta_{m,2}^{c(s)M-1} + B_m^{c(s)M-1} + \hat{B}_m^{c(s)M-1} \eta_{m,2}^{c(s)N-1} \quad 5.5$$

where

$$A_m^{c(s)M-1} = - (F_m^{c(s)M} + G_m^{c(s)M} A_m^{c(s)})^{-1} E_m^{c(s)M} \quad 5.6$$

$$B_m^{c(s)M-1} = - (F_m^{c(s)M} + G_m^{c(s)M} A_m^{c(s)})^{-1} (G_m^{c(s)M} B_m^{c(s)M} + H_m^{c(s)M}) \quad 5.7$$

$$\hat{B}_m^{c(s)M-1} = - (F_m^{c(s)M} + G_m^{c(s)M} A_m^{c(s)})^{-1} G_m^{c(s)M} B_m^{c(s)M} \quad 5.8$$

Introduce the matrices $A_m^{c(s)N,M}$, $B_m^{c(s)N,M}$, $\hat{B}_m^{c(s)N,M}$:

$$\eta_{m,2}^{c(s)M} = A_m^{c(s)N,M} \eta_{m,2}^{c(s)N} + B_m^{c(s)N,M} + \hat{B}_m^{c(s)N,M} \eta_{m,2}^{c(s)N-1} \quad 5.9$$

$$A_m^{c(s)N,M} = \prod_{K=N}^{M-1} A_m^{c(s)K}; \quad B_m^{c(s)N,M} = \sum_{L=N+1}^M A_m^{c(s)L,M} B_m^{c(s)L-1};$$

$$\hat{B}_m^{c(s)N,M} = \sum_{L=N+1}^M A_m^{c(s)L,M} \hat{B}_m^{c(s)L-1}; \quad A_m^{c(s)K,K} = I \quad 5.10$$

Hereafter for convenience in the quantities with the indexes $c(s)$ we admit these indexes. We will write these indexes only in quantities which are introduced for the first time.

Using the expressions (1.8, 3.3, 3.25, 4.1, 4.3+4.5, 4.9, 4.10) we express $\eta_{m,2}^{c(s)N}$ in terms of $\eta_{m,2}^{c(s)N}$ and $\vec{C}_m^{c(s)}$:

$$\begin{aligned} \eta_{m,2}^{c(s)N} = & \theta_1^{c(s)} \{ \tilde{\Lambda}_{m,t}^{c(s)} + i S_{m,1}^{c(s)} (h_m^{c(s)})^{-1} W_m^{c(s)} \}^{-1} \times \{ \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} \eta_{m,2}^{c(s)N} - \\ & - 2 S_{m,1}^{c(s)} \vec{C}_m^{c(s)} + \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{V}_m^{c(s)} - i S_{m,1}^{c(s)} (h_m^{c(s)})^{-1} V_m^{c(s)} + P_{m,2}^{c(s)} \} + \\ & + \theta_2^{c(s)} \{ S_{m,1}^{c(s)} \tilde{\Lambda}_{m,t}^{c(s)} W_m^{c(s)} + i (h_m^{c(s)})^{-1} \}^{-1} \times \{ S_{m,1}^{c(s)} \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} \eta_{m,2}^{c(s)N} - 2 \vec{C}_m^{c(s)} + \\ & + S_{m,1}^{c(s)} (\tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{V}_m^{c(s)} - \tilde{\Lambda}_{m,t}^{c(s)} V_m^{c(s)}) - P_{m,2}^{c(s)} \} \end{aligned} \quad 5.11$$

Here $h_m^{c(s)}$ is determined according to the rule (3.21). From (5.5) and (5.11) express $\eta_{m,2}^{c(s)N}$ through $\eta_{m,2}^{c(s)N-1}$ and $\vec{C}_m^{c(s)}$.

$$\eta_{m,2}^{c(s)N} = \hat{\Omega}_m^{c(s)} \eta_{m,2}^{c(s)N-1} + \tilde{\Omega}_m^{c(s)} \vec{C}_m^{c(s)} + \tilde{\Omega}_m^{c(s)} \quad 5.12$$

where

$$\hat{\Omega}_m^{c(s)} = \gamma_1^{c(s)} \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} \hat{B}_m^{c(s)} + \gamma_2^{c(s)} S_{m,1}^{c(s)} \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} \hat{B}_m^{c(s)} \quad 5.13$$

$$\tilde{\Omega}_m^{c(s)} = -2 (\gamma_1^{c(s)} S_{m,1}^{c(s)} - \gamma_2^{c(s)}) \quad 5.14$$

$$\begin{aligned} \tilde{\Omega}_m^{c(s)} = & \gamma_1^{c(s)} \{ \tilde{\Lambda}_{m,s}^{c(s)} (\overleftarrow{W}_m^{c(s)} \hat{B}_m^{c(s)} + \overleftarrow{V}_m^{c(s)}) - i S_{m,1}^{c(s)} (h_m^{c(s)})^{-1} V_m^{c(s)} + P_{m,2}^{c(s)} \} + \\ & + \gamma_2^{c(s)} \{ S_{m,1}^{c(s)} \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} \hat{B}_m^{c(s)} + S_{m,1}^{c(s)} (\tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{V}_m^{c(s)} - \tilde{\Lambda}_{m,t}^{c(s)} V_m^{c(s)}) - P_{m,2}^{c(s)} \} \end{aligned} \quad 5.15$$

$$\gamma_1^{c(s)} = \theta_1^{c(s)} \{ \tilde{\Lambda}_{m,t}^{c(s)} + i S_{m,1}^{c(s)} (h_m^{c(s)})^{-1} W_m^{c(s)} - \tilde{\Lambda}_{m,s}^{c(s)} \overleftarrow{W}_m^{c(s)} A_m^{c(s)} \}^{-1} \quad 5.16$$

$$Y_2^{(c)} = \Theta_2^{-1} \left\{ S_{m,1}^{-1} (\hat{\Lambda}_{m,t}^{N_c-2} W_m^{N_c-1} - \hat{\Lambda}_{m,s}^{N_c-2} A_m^{N_c-1}) + i(h_m^{N_c-1})^{-1} \right\}^{-1} \quad 5.17$$

Substituting (5.12) in (5.9) at $M=N_c-2$ and $N=1$ we get:

$$\eta_{m,2}^{N_c-2} = (A_m^{1,N_c-2} \hat{\Omega}_m + \hat{B}_m^{1,N_c-2}) \eta_{m,2}^{N_c-1} + A_m^{1,N_c-2} \Omega_m \vec{C}_m^1 + A_m^{1,N_c-2} \tilde{\Omega}_m + \tilde{B}_m^{1,N_c-2}$$

Using (1.8, 3.3, 3.25, 4.1, 4.3+4.5, 4.9, 4.10) we can write for

$$\eta_{m,2}^{N_c-1}, \eta_{m,2}^{N_c-2} \text{ and } \vec{C}_m^{N_c} \text{ the expression like (5.11):}$$

$$\left(\beta_1 \Theta_1^{-1} + \beta_2 \Theta_2^{-1} \right) \eta_{m,2}^{N_c-1} = \Theta_1^{N_c-1} \left\{ K_1 \eta_{m,2}^{N_c-2} + K_1 \vec{C}_m^{N_c} + \hat{K}_1 \right\} + \Theta_2^{N_c-1} \left\{ K_2 \eta_{m,2}^{N_c-2} + K_2 \vec{C}_m^{N_c} + \hat{K}_2 \right\} \quad 5.19$$

where

$$\beta_1^{(c)} = S_{m,t}^{N_c-1} \hat{\Lambda}_{m,t}^{N_c-1} W_m^{N_c-1} + i(h_m^{N_c})^{-1}; \quad \beta_2^{(c)} = \hat{\Lambda}_{m,t}^{N_c-1} + i S_{m,t}^{N_c-1} (h_m^{N_c})^{-1} W_m^{N_c-1} \quad 5.20$$

$$K_1^{(c)} = S_{m,t}^{N_c-1} \hat{\Lambda}_{m,s}^{N_c-1} \vec{W}_m^{N_c-2}; \quad \hat{K}_1^{(c)} = -2 \quad 5.21$$

$$\hat{K}_1^{(c)} = S_{m,t}^{N_c-1} (\hat{\Lambda}_{m,s}^{N_c-1} \vec{V}_m^{N_c-2} - \hat{\Lambda}_{m,t}^{N_c-1} V_m^{N_c-1}) + P_{m,2}^{N_c-1} \quad 5.22$$

$$K_2^{(c)} = \hat{\Lambda}_{m,s}^{N_c-1} \vec{W}_m^{N_c-2}; \quad \hat{K}_2^{(c)} = -2 S_{m,t}^{N_c-1} \quad 5.23$$

$$\hat{K}_2^{(c)} = \hat{\Lambda}_{m,s}^{N_c-1} \vec{V}_m^{N_c-2} - i S_{m,t}^{N_c-1} (h_m^{N_c})^{-1} V_m^{N_c-1} - P_{m,2}^{N_c-1} \quad 5.24$$

From (5.18) and (5.19) we obtain the dependence of $\eta_{m,2}^{N_c-1}$ on \vec{C}_m^1 and $\vec{C}_m^{N_c}$.

$$\eta_{m,2}^{N_c-1} = \Theta_1^{N_c-1} X_1^{(c)} \left\{ K_1 A_m^{1,N_c-2} \Omega_m \vec{C}_m^1 + \tilde{K}_1 \vec{C}_m^{N_c} + K_1 (A_m^{1,N_c-2} \hat{\Omega}_m + \hat{B}_m^{1,N_c-2}) + \hat{K}_1 \right\} +$$

$$+ \Theta_2^{N_c-1} X_2^{(c)} \left\{ K_2 A_m^{1,N_c-2} \Omega_m \vec{C}_m^1 + \tilde{K}_2 \vec{C}_m^{N_c} + K_2 (A_m^{1,N_c-2} \hat{\Omega}_m + \hat{B}_m^{1,N_c-2}) + \hat{K}_2 \right\} \quad 5.25$$

where

$$X_1^{(c)} = \left\{ \beta_1 - K_1 (A_m^{1,N_c-2} \hat{\Omega}_m + \hat{B}_m^{1,N_c-2}) \right\}^{-1} \quad 5.26$$

$$X_2^{(c)} = \left\{ \beta_2 - K_2 (A_m^{1,N_c-2} \hat{\Omega}_m + \hat{B}_m^{1,N_c-2}) \right\}^{-1} \quad 5.27$$

To determine the fields we can first determine $\eta_{m,2}^{N_c}$ from (5.25) and (5.12), then from (5.9) obtain $\eta_{m,2}^M$ for arbitrary M . Now using the formulae (4.5) we determine $Y_m^N(e^N)$ and $Y_m^N(0)$ for the arbitrary N , which is equivalent to the determination of the quantities $X_m^N(0)$ and $X_m^N(e^N)$. At known X^N and Y^N from formulae for field expression we obtain the fields in an arbitrary point of structure.

Appendix

We consider the practical case in which the charged bunches move parallel to the axis of structure: we assume that the motion of bunch is determined by the rule:

$$\rho(z, t, z, t) = \rho_0(z, \varphi, z - vt); \quad \vec{J} = \rho_0 \vec{V} \quad 1A$$

where

$$\vec{V} = (0, 0, V)$$

The solution of Maxwell equations in the absence of structure which corresponds to distribution (1A) has the form:

$$\vec{E}^Q = \vec{E}^Q(r, \varphi, z - vt); \quad \vec{H}^Q = \vec{H}^Q(r, \varphi, z - t) \quad 2A$$

Expanding E_z^Q and E_φ^Q in Fourier series in φ on the cylindrical wall and making the Fourier transformation of the time t we get:

$$E_z^Q(a^N, \varphi, z, \tilde{z}) = \sum_m \left[\tilde{E}_{z(\varphi), m}^Q(a^N, \tilde{z}) \cos(m\varphi) + \tilde{E}_{z(\varphi), m}^Q(a^N, \tilde{z}) \sin(m\varphi) \right] e^{i\tilde{z}z} \quad 3A$$

where

$$\tilde{z} = \frac{\omega}{c}; \quad \beta = \frac{v}{c}$$

we find the solution of homogeneous equations by introducing the Hertz vectors:

$$\Phi^{E(H), N} = \sum_m I_m(gz) e^{i\tilde{z}z} \left[\tilde{C}_m^{E(H), N} \cos(m\varphi) + \tilde{C}_m^{E(H), N} \sin(m\varphi) \right] \quad 4A$$

where $g = \tilde{z} \sqrt{1 - \beta^2}$; I_m - are the Bessel function of imaginary argument.

According to the formulae in the main text (1.1) and (1.2):

$$\left. \begin{aligned} E_z^E &= g^2 \sum_m I_m(gz) e^{i\tilde{z}z} \left[\tilde{C}_m^{E, N} \cos(m\varphi) + \tilde{C}_m^{E, N} \sin(m\varphi) \right] \\ E_\varphi^E &= \frac{i\tilde{z}}{z\beta} \sum_m I_m(gz) e^{i\tilde{z}z} \left[\tilde{C}_m^{E, N} \cos(m\varphi) - \tilde{C}_m^{E, N} \sin(m\varphi) \right] \\ E_z^H &= 0 \\ E_\varphi^H &= i\tilde{z}g \sum_m I_m'(gz) e^{i\tilde{z}z} \left[\tilde{C}_m^{H, N} \cos(m\varphi) + \tilde{C}_m^{H, N} \sin(m\varphi) \right] \end{aligned} \right\} 5A$$

Equating the total E_φ and E_z with nil on the cylindrical wall we obtain:

$$\tilde{C}_m^{E, N} = - \frac{\tilde{E}_{z, m}^Q(a^N, \tilde{z})}{g^2 I_m(ga^N)} \quad 6A$$

$$\tilde{C}_m^{H, N} = \frac{1}{g I_m'(ga^N)} \left[\frac{\tilde{E}_{z, m}^Q(a^N, \tilde{z})}{\beta a^N g^2} - \frac{\tilde{E}_{\varphi, m}^Q(a^N, \tilde{z})}{iK} \right] \quad 7A$$

$$\tilde{C}_m^{H, N} = - \frac{1}{g I_m'(ga^N)} \left[\frac{\tilde{E}_{z, m}^Q(a^N, \tilde{z})}{\beta a^N g^2} + \frac{\tilde{E}_{\varphi, m}^Q(a^N, \tilde{z})}{iK} \right] \quad 8A$$

At $v \rightarrow c$ the radial functions $R_m(r)$ are the solution of equation:

$$R'' + \frac{R'}{r} - \frac{m^2 R}{r^2} = 0 \quad 9A$$

The finite solutions at finite r are:

$$R_m(r) = C_m r^m \quad 10A$$

These functions we obtain also in the way:

$$\lim_{g \rightarrow 0} \frac{I_m(gz)}{g^m} = C_m z^m \quad 11A$$

Here C_m are constants. Now we can write:

$$\left(\frac{c(s)}{c_m} \right)_{v=c} = - \frac{c(s)}{c_{\varphi, m} (a^N, \tilde{k})} \quad 12A$$

In conclusion we give an example $\xi_{\varphi, m}^{(s)}(a^N, \tilde{k})$ for the more practical case at which point-like bunches move at $v \approx c$ parallel to the axis at the small distance δz^Q in the plane $\varphi = \varphi^Q$ (in linear approximation to $\delta z^Q/a^N$):

$$\xi_{\varphi, 1}^Q = \frac{2eN_B}{c(a^N)^2} \delta z^Q \cos \varphi^Q; \quad \xi_{\varphi, 1}^Q = \frac{2eN_B}{c(a^N)^2} \delta z^Q \sin \varphi^Q \quad 13A$$

In this approximation $\xi_{\varphi, m}^{(s)} = 0$ for all $m \neq 1$.

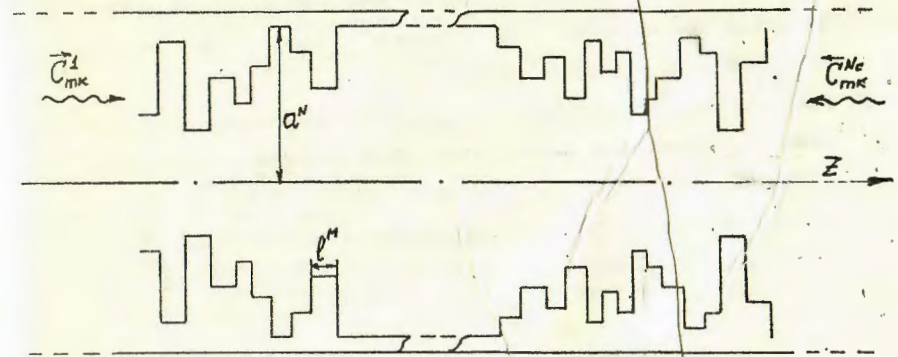


Рис. I Общий вид осевого разреза структуры и некоторые обозначения (размеры произвольны).

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Նախնատիպ ԵրՖԻ-1426(13)-94

ՉԼԱՆԱԶԵՎ ԲԱՆԱԶԵՎԵՐ ՈՉ ՊԱՐԲԵՐԱԿԱՆ ԿԱՌՈՒՑՎԱԾՔՆԵՐՈՒՄ
ՂԱՇՏԵՐԻ ԿԻՍԱՆԱԼԻՏԻԿ ՎԱՇՎԱՐԿՄԱՆ ՎՈՍԱՐ

Վ.Գ. ՎԱՍԲԱՐՇՈՒՄՅԱՆ

Էդրոս են բերված դաշտերի հաշվարկի բաղաձևեր ոչ պարբերական գլխաձև ալիքատարում:

Հաշվի են առնված նաև համակարգի առանցքին զուգահեռ $v \rightarrow c$ արագությամբ շարժվող արագացվող փնջով զրգոյված դաշտերը:

Բաղաձևերը ստացված են դաշտերի կարման եղանակով և արտահայտված են 'անցումային' մատրիցաների լեզվով:

Երևանի Ֆիզիկայի Ինստիտուտ
Երևան - 1994

Препринт ЕрФИ-1426(13)-94

ФОРМУЛЫ ДЛЯ ПОЛУАНАЛИТИЧЕСКИХ РАСЧЕТОВ ПОЛЕЙ
В ЦИЛИНДРИЧЕСКИХ АПЕРИОДИЧЕСКИХ СТРУКТУРАХ

В. Г. Амбарцумян

Выведены формулы для расчета полей в аperiodическом цилиндрическом волноводе.

Учтены также поля возбуждаемые пучком частиц движущихся параллельно оси структуры со скоростью $v \rightarrow c$.

Формулы получены методом свивки полей и выражены на языке матриц "переходов".

Ереванский Физический Институт